Reference Frames in Diffusion

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It is frequently necessary to convert diffusion equations from one reference frame to another (1, 2). In this note the transformation between two arbitrary reference frames is developed, and a few examples of interest in liquid systems are worked out.

The velocity of species i in an ncomponent mixture is written as

$$v_i = u_i^R + V^R \tag{1}$$

where the reference velocity is

$$V^{R} = \frac{\sum_{j=1}^{n} v_{j} \rho_{j} Z_{j}^{R}}{\sum_{j=1}^{n} \rho_{j} Z_{j}^{R}} = \frac{\sum_{j=1}^{n} n_{j} Z_{j}^{R}}{\sum_{j=1}^{n} \rho_{j} Z_{j}^{R}}$$
(2)

Multiplying Equation (1) by ρ_i one gets the mass fluxes

$$n_i = J_i^R + \rho_i V^R \tag{3}$$

and multiplying Equation (3) by Zin and summing one gets

$$\sum_{i=1}^n J_i^R Z_i^R = 0 (4)$$

In terms of the second reference velocity V^{R'} Equation (3) becomes

 $n_i = J_{iR'} + \rho_i \dot{V}^{R'}$ Equating (3) and (5) one gets

$$J_{i}^{R}-J_{i}^{R'}=\rho_{i}\left(V^{R'}-V^{R}\right) \qquad (6)$$

Multiplying Equation (5) by Z_i^R and summing, using Equation (2), one

$$V^{R'} - V^{R} = -\frac{\sum_{j=1}^{n} J_{j}^{R'} Z_{j}^{R}}{\sum_{j=1}^{n} \rho_{j} Z_{j}^{R}}$$
(7)

and combining with Equation (6)

$$J_{i}^{R} = J_{i}^{R'} - \rho_{i} \frac{\sum_{j=1}^{n} J_{j}^{R'} Z_{j}^{R}}{\sum_{j=1}^{n} \rho_{j} Z_{j}^{R}}$$
(8)

This is the desired relationship between the fluxes in the two coordinate systems.

The volume average velocity, which is of particular interest in liquid diffusion, is defined by letting $Z_{i}^{B'} = v_{i}$, the partial mass volume of species j. Equation (2) then defines the volume average velocity.

Measured binary diffusion coefficients are usually defined by

$$J_{i}^{\ \nu} = -D_{i}^{\ \nu} \nabla \rho_{i} \tag{9}$$

where superscript R' is now written as V, so J_i^{ν} is the flux with respect to the volume average velocity. Assuming constant Z_i^R , and substituting Equation (9) into (8), one gets

Equation (10) gives the flux with respect to the reference velocity given by Equation (2). For $Z_i^R = 1$ the reference velocity from Equation (2) is the mass average velocity

$$V^m = v_1 w_1 + v_2 w_2 \tag{11}$$

and the flux is

$$J_{i}^{m} = -D^{r} \rho \nabla w_{i} \qquad (12)$$

When $Z_i^R = 1/M_i$, the reference velocity is the molar average

$$V^{M} = v_{1}x_{1} + v_{2}x_{2} \tag{13}$$

and the molar flux with respect to this

$$\phi_i^{M} = J_i^{M}/M_i = -D^{\nu}C \nabla x_i$$
(14)

The relationship between Equations (9), (12), and (14) is given by Bird, Stewart and Lightfoot (1).

In multicomponent systems Equation (9) may be replaced by (2, 3, 4)

$$J_{i}^{\nu} = -\sum_{i=1}^{n-1} D^{\nu}_{ij} \nabla \rho_{j} \qquad (15)$$

which, with Equations (8) and (4),

$$J_{i}^{R} = -\sum_{i=1}^{n-1} \left[D^{V}_{i,i} + \frac{w_{i}}{\sum_{k=1}^{n} w_{k} Z_{k}^{R}} \sum_{j=1}^{n-1} \left(Z_{n}^{R} \frac{v_{j}}{\bar{v}_{n}} - Z_{j}^{R} \right) D^{V}_{j,i} \right] \nabla \rho_{i}$$
(16)

As before, with $Z_{i}^{R} = 1$ one gets the mass flux with respect to the mass average velocity

$$J_{i}^{m} = -\sum_{i=1}^{n-1} D^{m}_{ii} \nabla \rho_{i} \qquad (17)$$

$$D^{m_{li}} = D^{v_{il}} + w_{i} \sum_{j=1}^{n-1} \left(\frac{\overline{v_{j}}}{\overline{v_{n}}} - 1 \right) D^{v_{jl}}$$
(18)

and letting $Z_{i}^{R} = 1/M_{i}$ one gets the molar flux with respect to the molar average velocity

$$\phi_i = -\sum_{i=1}^{n-1} D^{\mathsf{M}}_{i\,i} \, \nabla \, C_i \qquad (19)$$

$$D^{M}_{ii} = \frac{M_{i}}{M_{i}} D^{V}_{ii} + x_{i} \sum_{j=1}^{n-1}$$

$$\left(\frac{\overline{V}_{i}}{\overline{V}_{i}}-1\right) \frac{M_{i}}{M_{i}} D^{\nu_{ji}} \qquad (20)$$

$$C_i = \rho_i/M_i$$
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NOTATION

= molar density

= velocity of species i with respect to reference velocity

= partial molal volume

= some weighted average of the individual velocities

= mass fraction w

= mole fraction

= weighing property

density ρ

= mass of species i per unit vol-

LITERATURE CITED

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